THIN LAYER MODELING AND DETERMINATION OF THERMODYNAMIC PROPERTIES OF TOMATO SLICES DURING HOT AIR DRYING

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Abstract: The drying kinetics and determination of thermodynamic properties of sliced tomato samples during hot air drying in a hybrid solar-electric crop dryer were presented. One kilogram batch of freshly harvested tomato samples were sliced to 10 mm thickness and dried at varying air velocities (1.0, 1.5 and 2.0 ms⁻¹) and temperatures (50, 55, 60, 65, and 70°C) using the hybrid mode. In order to choose the best drying model, eight thin-layer mathematical models were fitted to the experimental data. The high values of coefficient of determination, R² and the low values of reduced sum of squares error (SSE) and root mean square error (RMSE) indicated that the Midilli *et al.* model adequately described the drying process of tomato slices, with its highest R² (0.9999), lowest SSE (0.1136) and lowest value of RMSE (0.0212) at 70°C temperature and 2.0 ms⁻¹ air velocity. Arrhenius model was used to represent the drying constant as a function of temperature. The effective moisture diffusivity increased with increase in temperature and air velocity; with the highest value obtained at air velocity of 2.0 ms⁻¹ and temperature of 70°C, whereas it was lowest at air velocity of 1.0 ms⁻¹ and temperature of 50°C. The mean activation energy required to dry 1kg batch of 10 mm sliced tomato samples was 39.34 kJmol⁻¹. Enthalpy and Gibbs free energy values were found to decrease with increasing drying temperature as well as the entropy which also exothermically decreased with temperature. Recommendations for further studies were stated.

Keywords: Thermodynamic properties, drying kinetics, tomato slices, water desorption, activation energy.

INTRODUCTION

Tomato (*Lycopersicon esculentum* L.) is a perishable and seasonal crop generally grown and widely eaten in most countries including Nigeria. It is one of the valuable fruit vegetables which is economically rated to be the second most important vegetable crop after potato [1, 2]. In developing countries such as Nigeria, tomato is a seasonal product, characterized by being in good quality, rich in vitamins and minerals, high moisture (usually above 90% wet basis),

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low fats contents especially at harvest, excessive and cheap in their seasons and scarce, costly and in bad quality during out of seasons [3, 4]. In order to make it available on the market as long as possible after harvest, the products are most often subjected to the drying process.

Its drying is a highly energy intensive operation as a result of the relatively high moisture content at harvest; and for this reason, considerable amounts of energy is required to heat the drying air so as to bring down the high moisture content to a safe storage level (usually 5 – 15% w.b.) at a temperature range of 35 – 65°C [3, 4].

In order to analyze the drying behaviour of an agricultural product during drying process, the study of its kinetics in thin layers is essential [5, 6, 7, 8]. Mathematical modeling involves predicting and simulating drying behaviour of certain parameters and processes in a unified manner regardless of the control mechanism, through empirical and phenomenological models [9, 10]. Several mathematical models such as the Midilli *et al.* model, Page model, Newton model, Fick's-diffusion model, Logarithmic model, Henderson and Pabis model *etc.* have been used to describe the thin layer drying process of agricultural products. These models which describe the characteristics of a particular product being dried are used to estimate the drying time of several products and also to generalize drying curves needed for dryer design and process optimization. The study of thermodynamic properties in the drying process of agricultural products aims to proffer solutions to problems related to stability and optimization of process conditions [10, 11]. It is necessary for optimal designing and dimensioning of crop dryers and other devices in various processes of preservation of product quality as well as in the proper understanding and provision of information on energy exchanges between one state of equilibrium to the other [10, 12]. Given the above, this study is circumscribed to model the drying kinetics and determine the thermodynamic properties of tomato slices at varying drying temperatures.

MATERIAL AND METHODS

Theoretical principles

The plot of moisture ratio with drying time obtained from the experimental data was used to represent the drying kinetics of tomato slices; since the initial value for moisture ratio is unity for each of the experiments, the moisture ratio curve will explain the drying behaviour better than that of moisture content curve [13]. Therefore, the moisture ratio, MR was calculated from Equation (1a) as [14]:

$$MR = \frac{M_t - M_e}{M_o - M_e} = e^{-kt} \quad (1a)$$

Where: M_t = Moisture content at any time, t (% db.); M_e = equilibrium moisture content (% db.); and M_o = initial moisture content (% db.), t = drying time (mins.), k = drying constant (min^{-1}).

The values of M_e are relatively small when compared to M_t and M_o , and thus had negligible error [15, 16, 17], therefore the moisture ratio was calculated as Equation (1b):

$$MR = \frac{M_t}{M_o} \quad (1b)$$

The drying rate, DR was obtained as expressed in Equation (2) [1]:

$$DR = \frac{M_{t+dt} - M_t}{M_o - M_e} \quad (2)$$

Where: M_{t+dt} = moisture content (% wet basis, wb) at time $t+dt$; M_t = Moisture content at time, t (% wb); t = drying time (mins.).

The drying curves were fitted to eight commonly known thin-layer drying models as shown in Table 1. The best of fit was obtained by using three statistical parameters: coefficient of determination (R^2), reduced sum of squares errors (χ^2), and root mean square error (RMSE) expressed as Equations (3) – (5) [5-10, 13, 15]:

$$R^2 = 1 - \left[\frac{\sum_{i=1}^N (MR_{pre} - MR_{exp,i})^2}{\sum_{i=1}^N (MR_{pre} - MR_{exp,i})^2} \right] \quad (3)$$

$$\chi^2 = \sum_{i=1}^n \frac{(MR_{exp,i} - MR_{pred,i})^2}{N - m} \quad (4)$$

$$RMSE = \sqrt{\frac{\sum_{i=1}^N (MR_{pre} - MR_{exp,i})^2}{N}} \quad (5)$$

Where: $MR_{exp,i}$ = the i th experimental moisture ratio; $MR_{pred,i}$ = the i th predicted moisture ratio; N = number of observation; m = number of constants in the drying model; MR_{pre} = mean of predicted moisture ratio.

Table 1. Thin-layer drying models.

Model No.	Model name	Model equation	References
1	Lewis	$MR = e^{(-kt)}$	Zarein et al., 2013; Darvishi, 2012
2	Page	$MR = e^{(-kt^n)}$	Zarein et al., 2013; Darvishi, 2012
3	Henderson and Pabis	$MR = ae^{(-kt)}$	Zarein et al., 2013, Darvishi, 2012.
4	Modified Henderson and Pabis	$MR = ae^{(-kt)} + be^{(-gt)} + c(e^{-ht})$	Zarein et al., 2013; Sahari and Driscoll, 2013
5	Logarithmic	$MR = a \exp(-kt) + c$	Zarein et al., 2013
6	Two-term	$MR = ae^{(-k_0t)} + be^{(-k_1t)}$	Sahari and Driscoll, 2013
7	Verma et al.	$MR = ae^{(-kt)} + (1 - a)e^{(-gt)}$	Karathanos, 1999; Darvishi, 2012.
8	Midilli et al.	$MR = ae^{(-kt^n)} + bt$	Zarein et al., 2013, Darvishi, 2012.

The effective moisture diffusivity (D_e) of food materials characterizes their intrinsic property of mass and moisture transport including molecular diffusion, vapour diffusion, hydrodynamic flow and other mechanisms [2, 18]. Moisture transfer (water transport) during drying agricultural crops takes place through molecular diffusion, and was described using the solution term of the simplified Fick's second law of diffusion expressed in Equations (6a) and (6b) as [5, 6, 19]:

$$MR = \frac{M_t - M_e}{M_0 - M_e} = \frac{8}{\pi} e^{\left(\frac{-\pi^2 D_e t}{L^2}\right)} \quad (6a)$$

$$\ln(MR) = \ln \frac{8}{\pi} - \frac{\pi^2 D_e t}{L^2} \quad (6b)$$

Where: MR = moisture ratio; D_e = effective moisture diffusivity ($m^2 s^{-1}$); L = half thickness of the sliced tomato samples (mm); t = drying time (mins).

The D_e was calculated, using the method of slopes as described by [5, 6, 19, 20]. A straight line was obtained when the logarithm of moisture ratio ($\ln MR$) was plotted against drying time (t) for different temperatures and air velocities at constant slice thickness. The slope (coefficient k_1) of the regression line is related to the effective diffusion coefficient (D_e) of sliced tomato samples to be determined by substitution into Equation (7) as [19]:

$$k_1 = \frac{\pi^2 D_e}{4L^2} \quad (7)$$

The activation energy (E_a) was calculated by applying the drying constant (k_d) of the best fitted model to the Arrhenius as expressed in Equation (8) [1, 19]:

$$K_d = A_o e^{\left(-\frac{E_a}{R_g T_a}\right)} \quad (8)$$

The plots of the logarithm of the drying constant ($\ln K_d$) against the reciprocal of the absolute drying temperature (T_a^{-1}) gave a linear function expressed as Equation (9) [6, 19]:

$$\ln K_d = \ln A_o - \frac{E_a}{R_g T_a} \quad (9)$$

Where: K_d = drying constant = effective moisture diffusion coefficient ($m^2 s^{-1}$); A_o = pre-exponential factor ($m^2 s^{-1}$); E_a = activation energy of diffusion of water ($kJ mol^{-1}$); R_g = gas constant ($8.3143 kJ mol^{-1} K$); T_a = absolute temperature ($^{\circ}K$).

Substituting the slope of the linear function, $k_2 = \frac{E_a}{R_g}$ into Equation (9) yields the activation of the slice tomato samples expressed as Equation (10):

$$E_a = k_2 \cdot R_g \quad (10)$$

The coefficient of determination (R^2) of the model equation was obtained by fitting Equation (9) into the experimental data using linear regression (Minitab version 17). The thermodynamic properties of the drying process of tomato slice in a hybrid solar-electric crop dryer were determined through method described by [10, 11] expressed as Equations (11) to (13):

$$\Delta H = E_a - R T_a \quad (11)$$

$$\Delta S = R \left(\ln A_o - \ln \frac{K_B}{h_p} - \ln T_a \right) \quad (12)$$

$$\Delta G = \Delta H - T_a \Delta S \quad (13)$$

Where: ΔH = enthalpy variation ($J mol^{-1}$); ΔS = entropy variation ($J mol^{-1} K^{-1}$); ΔG = Gibbs free energy variation ($J mol^{-1}$); K_B = Boltzmann constant ($1.38 \times 10^{-34} Js^{-1}$); h_p = Planck constant ($6.626 \times 10^{-34} Js^{-1}$); T_a = absolute temperature ($^{\circ}K$).

Experimental procedure

Drying experiment was performed using a hybrid solar-electric convective dryer (Figure 1) designed and developed in the Engineering Workshop of Federal University of Technology, Owerri, Nigeria. A local variety of fresh tomato samples (*Gboko Spp.*) were procured from a rural market in Owerri, Imo State of Nigeria. The samples were washed and sliced into 10 mm thickness size using a sharp stainless steel knife and a vernier caliper with the direction of cutting perpendicular to the vertical axis of the tomato samples. The dryer heating unit (1500 W) was switched on, the required air flow and temperature were initiated by the 4 x 4 matrix keypad of the control unit. The drying chamber (with dimensions: 40 cm x 40 cm x 50 cm) was allowed to maintain steady-state condition. When the optimum preset drying temperature was attained, the arduino microprocessor automatically switches off the heating unit, and turns it on again when the drying chamber temperature falls one degree below the preset temperature. The dryer was programmed to operate at five different temperature thresholds of 50, 55, 60, 65 and 70 $^{\circ}C$, and at three varying air velocities (1.0, 1.5 and 2.0 ms^{-1}).

Figure 1. Isometric view of the hybrid drying system.

The initial mass of the 1 kg batch sliced samples was measured by a digital weighing balance (0.01 g, Camry instruments, China) and recorded, and placed on the drying racks in such a way that the drying air flows axially into the sample matrix (for faster drying). The initial moisture content of the samples was measured by drying 20 g of representative sliced sample in an oven dryer set at 105°C for 24 hours [8, 21, 22]. At every 30 minutes time interval, the control unit of the dryer system (consisting of arduino microprocessor) measures, records and displays on the screen, sample weight loss as well as the drying temperatures and relative humidities of the drying racks, chimney, solar collector, and ambient environment. The difference between the initial dried mass and the 30-minutes interval measured masses were used to calculate the moisture content at any time, t as well as the percentage weight loss for each dried batch. The weight losses were recorded by the use of a weight sensor attached to the weighing balance (with a precision of 0.01 g) in the drying chamber. The experiment was repeated for varying sample thicknesses, temperatures and air velocities for a batch of 1000 g. Drying was stopped when variation in the mass of tomato samples on the drying racks remained approximately constant, thus hygroscopic equilibrium was achieved. At this point moisture content decreased from 94.7% to 12.5% (w.b.).

RESULTS AND DISCUSSION

Modeling of drying curves

The kinetics of water desorption in tomato slices was investigated using the moisture content data (for 50, 55, 60, 65 and 70°C temperatures; 1.0, 1.5, and 2.0 ms^{-1} air velocities; and constant slice thickness of 10 mm) converted to moisture ratio using Equation (1b) and then fitted to the eight drying models (Table 1). Amongst the evaluated models, Midilli model showed the best fit to the experimental data of moisture ratio for all air velocity and temperature levels, having the highest mean values of R^2 of 0.9996 and lowest mean values of χ^2 (0.1814) and (0.00298) RMSE. The Midilli model had the highest value of R^2 , and lowest values for χ^2 and RMSE at 2.0 ms^{-1} air velocity as shown in Table 2. At all temperature levels, the values obtained with the Midilli model satisfied the criterion for goodness of fit: highest value of R^2 (0.9999), lowest value of $\chi^2 = 0.1136$, and lowest value of RMSE = 0.0212 at 70°C temperature and 2.0 ms^{-1} air velocity. The best fitted drying model describing the drying behaviour of sliced tomato samples (at air velocity of 2.0 ms^{-1} and temperature of 70°C) in a hybrid solar-electric dryer is therefore expressed as Equation (14):

$$\text{MR}_{\text{tomato}} = 4.926e^{(-0.8041t^{1.322})} + 0.007t \quad [R^2 = 0.9999] \quad (14)$$

Table 2. Statistical results obtained from the eight considered drying models at 2.0 ms^{-1} air velocity and varying drying temperatures.

Model name	Temp. 50°C			Temp. 55°C			Temp. 60°C		
	R^2	χ^2	RMSE	R^2	χ^2	RMSE	R^2	χ^2	RMSE
Lewis	0.9987	2.5233	0.0242	0.9990	2.4218	0.0242	0.9996	2.4129	0.0218
Page	0.9959	0.6723	0.00692	0.9961	0.6719	0.00653	0.9973	0.6231	0.00601
Henderson and Pabis	0.9976	1.9273	0.0102	0.9981	1.9201	0.0100	0.9981	1.8407	0.00945
Modified Henderson and Pabis	0.9921	3.293	0.0197	0.9930	3.242	0.0181	0.9936	3.118	0.0174
Logarithmic	0.9985	0.8763	0.00722	0.9986	0.8701	0.00711	0.9989	0.8614	0.00703
Two-term	0.9955	0.7233	0.00726	0.9958	0.7015	0.00701	0.9962	0.6821	0.00631
Verma et al.	0.9961	2.649	0.0273	0.9961	2.602	0.0220	0.9966	2.531	0.0171
Midilli et al.	0.9993	0.2114	0.00438	0.9995	0.2106	0.00316	0.9997	0.1931	0.00281

Model name	Temp. 65°C			Temp. 70°C		
	R^2	χ^2	RMSE	RMSE	R^2	χ^2
Lewis	0.9993	2.3704	0.02133	0.9996	2.2014	0.0198
Page	0.9980	0.5831	0.00601	0.9987	0.5704	0.00549
Henderson and Pabis	0.9984	1.8114	0.00945	0.9989	1.7931	0.00724
Modified Henderson and Pabis	0.9941	2.504	0.0169	0.9944	2.894	0.0149
Logarithmic	0.9991	0.8401	0.00698	0.9994	0.8277	0.00684
Two-term	0.9966	0.6328	0.00622	0.9969	0.6014	0.00619
Verma et al.	0.9972	2.217	0.0136	0.9974	2.109	0.0149
Midilli et al.	0.9998	0.1783	0.00243	0.9999	0.1136	0.00212

Equation (15) was validated by plotting the values of the predicted moisture ratios against those of the experimental and is presented in Figure 2. The high coefficient of determination ($R^2 = 0.9998$) which is close to unity, as well as the closeness of the points to the dotted lines indicate strong correlation or equality between the predicted and experimental values. Thus the suitability of the model to describe the drying behaviour of tomato slices in a convective hybrid solar-electric dryer. The behaviour of moisture ratio as a function of the drying time of tomato slices under the selected temperature levels at constant slice thickness is as shown in Figure 3.

Figure 2. Predicted and experimental moisture ratio values for the Midilli model at 2.0 ms^{-1} and 70°C temperature.

Figure 3. Drying curves of tomato slices described by Midilli *et al.* model at 2.0ms^{-1} and varying temperature levels.

However, in the context of thin-layer drying models, [16] evaluated the drying of tomato samples and found that the Midilli *et al.* model was the most suitable to describe the drying process at temperature range of 20, 40 and 60°C and at a constant air velocity of 2.0ms^{-1} . Similarly, [23] in drying of lemon grass leaves observed that Midilli *et al.* model was the best in describing the drying process at a temperature range of 30 to 60°C . [24] found also that Midilli *et al.* was adequate in describing the drying process of Cumari do Para pepper (*Capsicum chinense Jacqui*) at temperatures of 45, 55 and 65°C . All these corroborated with the present study.

Figure 3 illustrates that the higher the drying temperature, the shorter the drying time. This is as a result of increased kinetic energy of internal water molecules to diffuse and evaporate at higher rates from the interior and surface of the products to the ambient air respectively. This thus, increases the drying rate and reduces the drying time. This is in agreement with the findings of [25], in thin-layer drying of jujube fruits; [19] in drying of ginger slices; [6, 19] for okra slices; [1] for tomato slices; [5] in drying of carrot slices. There is a sharper decrease in the moisture ratio at the beginning of the drying process, which could probably be as a result of the high initial moisture content of the tomato samples (94.7% w.b), which increases moisture loss. According to [26], this occurs when the moisture content of the product sample exceeds 80% w.b., the internal resistance to water transport is usually lower than the external resistance to moisture removal from the sample surface to ambient/drying air, which marks the constant rate period. Owing to that, there is internal resistance to moisture diffusion and the mechanism for controlling the drying process is by diffusion. [26, 27] suggest that in this drying period, the decreasing rate of the product internal moisture corresponds to the internal water migration that make up the drying kinetics.

The drying constants, K_d for the Midilli *et al.* model at different temperatures are given in Table 3. The natural logarithm of the drying constant, $\ln(K_d)$ is described as a function of the reciprocal of the absolute temperature, T_a^{-1} as presented in Figure 4. K_d increases in absolute values with temperature, due to greater heat transfer coefficient from the air to the product and, there is an increase in moisture diffusion to the product surface as a result of increased air velocity and temperature. The variations in the model parameters (a , n and b) are more related to mathematical fits than to a drying phenomenon, since Midilli is a semi-empirical model [26, 28].

Table 3. K_d -values of the fitted drying model for different temperatures.

Temperature ($^{\circ}\text{C}$)	Midilli et al. model	R^2
50	$MR_{\text{tomato}} = 2.974e^{(-0.3074t^{1.202})} + 0.007t$	0.9993
55	$MR_{\text{tomato}} = 3.112e^{(-0.4011t^{1.196})} + 0.007t$	0.9995
60	$MR_{\text{tomato}} = 3.621e^{(-0.49918t^{1.22})} + 0.007t$	0.9997
65	$MR_{\text{tomato}} = 4.824e^{(-0.6083t^{1.282})} + 0.007t$	0.9998
70	$MR_{\text{tomato}} = 4.926e^{(-0.8041t^{1.322})} + 0.007t$	0.9999

Figure 4. Arrhenius-type relationship between drying rate and absolute temperature of sliced tomato samples at constant air velocity and slice thickness.

The linear regression of the relationship between the logarithm of the drying constant and the inverse of the absolute temperature is expressed in Equation (15) as:

$$\ln K_d = 14.863 - \frac{5.1815}{T_a} \quad [R^2 = 0.9967] \quad (15)$$

The high R^2 -value (0.9967) indicates strong correlation between the parameters of the linear regression function. The moisture diffusivity, D_e was calculated by substituting the values of Equation (7) into Equation (6b) and presented in Table 4. From Figure 4, the Arrhenius expression (Equation 8) can be written as:

$$K_d = 724328.28 \exp\left(\frac{38382.22}{8.3143T_a}\right) \quad (16)$$

Table 4. Effective moisture diffusivity (D_e) of tomato slices in different drying temperature and constant air velocity and sample thickness.

Air velocity (ms^{-1})	Diffusion coefficient (m^2s^{-1})				
	50 $^{\circ}\text{C}$	55 $^{\circ}\text{C}$	60 $^{\circ}\text{C}$	65 $^{\circ}\text{C}$	70 $^{\circ}\text{C}$
1.0	4.9541×10^{-9}	5.4729×10^{-9}	5.9156×10^{-9}	6.3817×10^{-9}	6.8153×10^{-9}
1.5	5.1495×10^{-9}	5.8182×10^{-9}	6.2457×10^{-9}	6.5041×10^{-9}	7.1163×10^{-9}
2.0	5.2364×10^{-9}	6.1922×10^{-9}	6.3343×10^{-9}	6.9932×10^{-9}	7.5726×10^{-9}

The D_e values fall within the reported range for vegetables and other food materials [6, 13, 16, 17, 29, 30, 31]. Moisture diffusivity was affected by the drying temperature and air velocity: D_e values increased with increasing air temperature due to decrease in vapour pressure in the product matrix [32, 33]. The minimum value of D_e ($4.9541 \times 10^{-9} \text{ m}^2\text{s}^{-1}$) was found at the minimum temperature, while at constant temperature values an increase in the air velocity increased D_e values probably because at a low air velocity (say 0.1 ms^{-1}), the drying air may had better contact with the sample surface but the rate of its heat and mass transfer was low as to necessitate greater absorption of moisture which results in decreased moisture diffusivity.

Similar observations were reported by other researchers for carrot, berberis fruit, red chillies, apples, okra, ginger, tomato, bell pepper, melon, and field pumpkin [1, 2, 13, 14, 15, 17, 19, 30, 34, 35, 36].

The slope of Figure 4 provides the relationship between E_a and R_g , whereas the intersection with the $\ln(K_d)$ -axis indicates the A_o -values. Table 5 shows that E_a -values and their corresponding R^2 and the pre-exponential factor values of the sliced tomato samples are within the range of E_a -values for food materials (12.7 to 110 kJmol⁻¹) as reported by [1, 5, 14, 19].

Table 5. Activation energy, pre-exponential factor and R^2 -values of tomato slices at varying air velocities.

Air velocity (ms ⁻¹)	E_a (kJmol ⁻¹)	R^2	$A_o \times 10^{-3}$ (m ² s ⁻¹)
1.0	40.96	0.9692	8.62
1.5	39.21	0.9703	7.07
2.0	37.86	0.9734	6.31
Mean	39.342	0.971	7.333

From Table 5, the activation energy, E_a of sliced tomato samples decrease with increasing air velocity. The E_a -values obtained from this present study are within the range (33.33 to 43.23 kJmol⁻¹) obtained by [16] for similar air velocity and temperature ranges. The high E_a -values were as a result of the relatively small amount of water removed by the thermal energy of the drying air. Activation energy is the energy barrier that must be overcome in order to initiate moisture diffusion. By increasing the temperature and drying rate (air flow), this energy barrier can be easily overcome but there should be a compromise between drying temperature and acceptable product quality [13]. Increasing the air velocity (at increased temperature) speeds up the rate of surface moisture evaporation, and most importantly increases the heat transfer rate which in turn increases the kinetic energy of the internal moisture for rapid collision, hence reduced activation energy. The mean E_a -value obtained from Figure 4 at varying air velocities was 38.38 kJmol⁻¹. Correa *et al.* [37] corroborated that the lower the E_a , the higher will be the water diffusivity in the product sample, i.e., the lower will be the energy necessary for physical transformation to occur, which refers to the transformation of liquid free water to vapour (drying). Similar observations were reported in the works of [6, 13, 16, 17] for sliced food materials.

Thermodynamically, E_a is defined as the ease with which water molecules surpass the energy barrier during internal moisture diffusion [26, 38]. The thermodynamic properties of sliced tomato drying were determined using Equations (11) to (13), and presented in Table 6.

Table 6. Thermodynamic properties of dried sliced tomato.

Temperature (°C)	ΔH (Jmol ⁻¹)	ΔS (Jmol ⁻¹)	ΔG (Jmol ⁻¹)
50	35695.45	-64.14	14968.61
55	35653.88	-64.05	14635.87
60	35612.31	-63.89	14327.36
65	35570.74	-63.77	14006.34
70	35529.17	-63.65	13687.67

Enthalpy decreased with increasing temperature, implying a lower energy requirement for drying of sliced tomato at higher drying temperatures. The positive values of the enthalpy, ΔH indicate that the drying process is an endothermic reaction, which requires addition or supply of energy in the form of heat for the physico-chemical transformations to occur. As the temperature of the drying chamber increased, entropy of the system also decreased; indicating increase in the order of the system, which is entropically unfavourable [26].

Some researchers [26, 39] suggest that a substance such as water can have only entropy if the degrees of freedom of the movement of translation or rotation are lost. Gibbs free energy (free enthalpy) is a thermodynamic potential of a system that can be considered as a measurement of maximum reversible work performed by a thermodynamic system in the process of moisture adsorption or desorption (i.e., moisture gain or loss) [26, 40]. According to Costa *et al.* [26], Gibbs energy provides clearer understanding of the thermodynamic driving forces that affect reactions.

However, in the drying of tomato slices, the effect of enthalpy was evident; which decreased with increasing drying temperatures, with its maximum ($14968.61 \text{ kJmol}^{-1}$) corresponding with the minimum temperature (50°C) and its positive values indicating endergonic reactions: supply of heat energy from the ambient environment – drying chamber, in which the sliced samples are kept for heat and mass reactions to occur.

CONCLUSION

Thin-layer mathematical modeling and determination of thermodynamic properties of sliced tomato samples during hot air drying in a hybrid solar-electric dryer were investigated at five different drying temperatures ($50, 55, 60, 65$ and 70°C), three different air velocities ($1.0, 1.5$ and 2.0 ms^{-1}), and at a constant slice thickness (10 mm). The following results were obtained as summarized below:

1. According to statistical analyses applied to the eight selected models, the Midilli et al. model gave the best fit to the experimental data of drying of tomato slices with the highest value of R^2 (0.9999), lowest value of $\chi^2 = 0.1136$, and lowest value of $\text{RMSE} = 0.0212$ at 70°C temperature and 2.0 ms^{-1} air velocity.
2. The model equation is expressed as: $\text{MR}_{\text{tomato}} = 4.926e^{(-0.8041t^{1.322})} + 0.027t$
3. The drying constant increased with increases in drying temperature. Temperature and air velocity influenced both moisture diffusivity and activation energy. The value of moisture diffusivity increased with increase in temperature and air velocity. The highest effective moisture diffusivity was observed at air velocity of 2.0 ms^{-1} and temperature of 70°C , whereas it was lowest at air velocity of 1.0 ms^{-1} and temperature of 50°C .
4. The activation energy of sliced tomato decreased with air velocity. The mean activation energy required to drying 1 kg batch of 10 mm sliced tomato samples in a hybrid solar-electric dryer is 39.34 kJmol^{-1} .
5. The effects of different drying temperatures on the thermodynamic properties of dried tomato slices such as enthalpy, entropy and, Gibbs free energy were studied. Enthalpy and Gibbs free energy decreased with increase in temperature, as well as entropy which exothermically decreased with increasing temperature.

Further studies on optimization of the drying process and determination of thermodynamic properties of different varieties of sliced fruits and vegetables at varying air velocities, sample thicknesses and drying temperatures using different drying systems are recommended. Experimental investigation on the heat and mass transfer parameters as well as the thermal utilization efficiency and dried product quality assessment of various species of sliced vegetables, roots and tuber crops using any solar-assisted hybrid dryer with a heat recovery unit is of great importance for future work.

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MODELI I TERMODINAMIČKE OSOBINE TANKIH KRIŠKI PARADAJZA SUŠENOG VRELIM VAZDUHOM

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Sažetak: Prikazana je kinetika sušenja i određivanje termodinamičkih osobina uzoraka narezanog paradajza tokom sušenja toplim vazduhom u solarnoj sušari. 1 kg svežih uzoraka paradajza su rezane na debljinu 10 mm i sušene na različitim brzinama vazduha (1,0, 1,5 i 2,0 ms⁻¹) i temperaturama (50, 55, 60, 65 i 70 °C) hibridnim načinom sušenja. Da bi se izabrao najbolji model sušenja, urađeno je 8 tanko-slojnih matematičkih modela sa eksperimentalnim podacima. Visoke vrednosti koeficijenta determinacije, R² i male vrednosti smanjene sume kvadrata greške (SSE) i kvadratne greške (RMSE) ukazuju da su Midilli i sar. model adekvatno opisali proces sušenja narezanog paradajza, sa najvišim R² (0.9999), najnižim SSE (0.1136) i najnižom vrednosti RMSE (0.0212) pri temperaturi od 70°C i brzinom vazduha 2.0 ms⁻¹. Arrhenius model predstavlja konstantu sušenja kao funkciju temperature. Efikasna difuzivnost vlage se povećava sa povećanjem temperature i brzine vazduha; sa najvećom vrednošću u dobijenom brzinom vazduha od 2,0 ms⁻¹ i temperaturom od 70°C, dok je bila najmanja brzina vazduha od 1,0 ms⁻¹ i temperatura od 50°C. Srednja energija aktivacije koja je potrebna za sušenje 1kg šarže od 10 mm rezanih uzoraka paradajza bila je 39,34 kJmol⁻¹. Utvrđeno je da se smanjuju vrednosti slobodne energije Enthalpy i Gibbs sa povećanjem temperature sušenja, kao i entropijom koja je takođe ekzotermno smanjena sa temperaturom. Navedene su preporuke za dalje istraživanje.

Ključne reči: termodinamička osobine, kinetika sušenja, rezanci paradajza, desorpcija vode, energija aktivacije.

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